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Density, Speed of Sound, Refractive Index, and Viscosity of 1-Amino-2-Propanol {or Bis(2-hydroxypropyl)amine} + Triethanolamine + Water from T = (288.15 to 333.15) K

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ABSTRACT: The density, speed of sound, refractive index, and viscosity of ternary systems formed by 1-amino-2-propanol (MIPA) {or bis(2-hydroxypropyl)amine (DIPA)} + triethanolamine (TEA) + water were determined at several temperatures from T = (288.15 to 333.15) K. The ternary systems analyzed in present work use different total amine concentrations of 5, 10, and 20 % (in volume), and the ratio between amine concentrations, in the nonaqueous fraction, was varied in the entire composition range. The excess volume was determined using the density experimental data for each mixture taking into account the DIPA melting point.



INTRODUCTION

The removal of acid gas impurities such as CO_2 and H_2S from natural, refinery, and synthesis gas streams is an important operation in gas processing. The main objective of these processes is to minimize the environmental pollution and, specifically, the greenhouse effect.

The amines that have proved to be of commercial interest for acid gas removal by chemical absorption are monoethanolamine (MEA), diethanolamine (DEA), and *N*-methyldiethanolamine (MDEA). Other amines, such as bis(2-hydroxypropyl)amine (DIPA), 1-amino-2-propanol (MIPA), or 3-amino-1-propanol (AP), have also been used, and some papers about this kind of processes have been published¹⁻³ in the past few years. The use of mixed amine solvents in gas-treating processes is of increasing interest nowadays.⁴⁻⁶ Blends of primary and tertiary amines (such as mixtures of MEA + MDEA or piperazine (PZ) + TEA) or secondary and tertiary amines (such as mixtures of DEA and MDEA) combine the high carbon dioxide loading of the tertiary amine, and for these reasons, they have been suggested for industrial gas-treating processes.⁷⁻⁹

The characterization of new mixtures for gas-liquid absorption processes is an important step that allows the analysis and evaluation of mass transfer and carbon dioxide capture capacity^{10,11} on the basis of these physical properties. For this reason, in this work, several physical properties (density, speed of sound, refractive index, and viscosity) of tertiary systems using blends of two amines: MIPA (or DIPA) with TEA, were measured over the temperature range employed in this work, (288.15 to 333.15) K. Previous studies have analyzed binary systems involving components used in this work.^{12–14} The present study includes the analysis of the influence of composition and temperature upon the previously commented physical properties.

EXPERIMENTAL SECTION

Materials. Table 1 shows the sample descriptions used in present work. The reagents were used without further purification.

Table 1. Sample Description Table

chemical name	source	initial mole fraction purity
MIPA ^a	Merck	≥ 0.98
$DIPA^{b}$	Sigma-Aldrich	≥ 0.98
TEA^{c}	Panreac	0.98
^a 1-Amino-2-propanol.	^b Bis(2-hydroxypropyl)amine. ^c Triethanolamine.

Samples were prepared individually from pure components before the measurement of different physicochemical properties. The uncertainty of the samples preparation in mole fraction was \pm 0.0008. Double-distilled water was used to prepare the amine aqueous solutions.

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Table 2. Comparison between Density ρ , Speed of Sound *c*, Viscosity η , and Refractive Index n_D Experimental and Literature Data for Pure Components^{*a*}

	ρ/ε	g⋅cm ⁻³	c/1	$n \cdot s^{-1}$	$\eta/\mathrm{mPa}\cdot\mathrm{s}$		n _D	
T/K	exp	lit.	exp	lit.	exp	lit.	exp	lit.
298.15	1.1210	1.1215 ¹⁵ 1.1208 ¹⁶	1611.5	TEA 1610.5 ¹⁶	605.95	607.0 ¹⁴	1.4832	1.4835 ¹⁵
298.15	0.9563	0.95651 ¹³ 0.95640 ¹⁷	1544.1	MIPA 1544.1 ¹⁷	24.234	26.685 ¹⁸	1.4461	1.44609 ¹⁸
				DIPA				
323.15	0.9841	0.98490 ¹⁶	1414.2		125.65	125.73 ¹⁶	1.4512	
^a Standard unc	ertainties <i>u</i> are a	u(T) = 0.01 K, u(p)	v) = 20 Pa, $u(x)$) = 0.0008, and the	he combined ex	panded uncertaintie	es $U_{\rm c}$ (level of c	confidence =0.95,

k = 2) are $U_c(\rho) = 2 \cdot 10^{-4} \text{ g cm}^{-3}$, $U_c(c) = 1.2 \text{ m s}^{-1}$, $U_c(\eta) = 0.0026 \text{ mPa·s}$, and $U_c(n_D) = 1.3 \cdot 10^{-4}$.

Table 3. Density ρ of MIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 333.15) \text{ K at } p = 10^5 \text{ Pa}^a$

					T_{\prime}	/K			
x_1	<i>x</i> ₂	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			A	mine Total Conc	entration $= 5 \% v$	rol			
0.0126	0.0000	0.9993	0.9983	0.9970	0.9956	0.9939	0.9920	0.9877	0.9826
0.0094	0.0018	1.0011	1.0001	0.9989	0.9974	0.9957	0.9938	0.9896	0.9845
0.0064	0.0035	1.0031	1.0021	1.0008	0.9993	0.9976	0.9958	0.9915	0.9854
0.0033	0.0048	1.0050	1.0040	1.0028	1.0013	0.9996	0.9977	0.9933	0.9876
0.0016	0.0055	1.0059	1.0049	1.0036	1.0021	1.0004	0.9985	0.9943	0.9877
0.0000	0.0064	1.0068	1.0058	1.0046	1.0031	1.0014	0.9995	0.9950	0.9886
			Ar	nine Total Conce	entration = 10 % v	vol			
0.0260	0.0000	1.0001	0.9990	0.9976	0.9959	0.9941	0.9921	0.9875	0.9822
0.0196	0.0034	1.0039	1.0027	1.0013	0.9997	0.9979	0.9959	0.9912	0.9859
0.0132	0.0067	1.0081	1.0069	1.0055	1.0039	1.0021	1.0001	0.9947	0.9888
0.0066	0.0101	1.0109	1.0098	1.0084	1.0068	1.0050	1.0030	0.9986	0.9925
0.0033	0.0116	1.0126	1.0115	1.0101	1.0085	1.0067	1.0047	1.0004	0.9943
0.0000	0.0134	1.0148	1.0136	1.0122	1.0106	1.0089	1.0069	1.0023	0.9962
			Ar	nine Total Conce	entration = 20 % v	vol			
0.0565	0.0000	1.0030	1.0014	0.9996	0.9975	0.9954	0.9930	0.9878	0.9821
0.0429	0.0073	1.0099	1.0083	1.0065	1.0046	1.0024	1.0001	0.9950	0.9894
0.0285	0.0150	1.0167	1.0152	1.0135	1.0116	1.0095	1.0072	1.0022	0.9967
0.0145	0.0218	1.0240	1.0226	1.0209	1.0190	1.0170	1.0147	1.0096	1.0038
0.0078	0.0256	1.0274	1.0259	1.0242	1.0224	1.0203	1.0181	1.0134	1.0080
0.0000	0.0294	1.0309	1.0294	1.0278	1.0260	1.0240	1.0218	1.0173	1.0112
a_{x_1} and x_2 are combined expansion.	the mole fract anded uncertai	ions of MIPA a inty U _c (level o	nd TEA, respec f confidence =	ctively. Standar 0.95, k = 2) is	d uncertainties s $U_c(\rho) = 2.10^{\circ}$	u are u(T) = 0 $u \operatorname{are } u(T) = 0$ $g \cdot \operatorname{cm}^{-3}$.	.01 K, $u(p) = 2$	0 Pa, $u(x) = 0$.	0008, and the

Methods. Density and Speed of Sound. The density (ρ) of pure components and the mixtures of different compounds were measured with an Anton Paar DSA 5000 vibrating tube densimeter and sound analyzer which was calibrated with ultrapure water and dry air. The glass vibrating-tube was carefully rinsed with filtered ethanol, acetone, and dry air before being loaded with the samples. The uncertainty in the density and speed of sound measurements was $\pm 5 \cdot 10^{-5}$ g·cm⁻³ and ± 0.8 m·s⁻¹, respectively.

Viscosity. The kinematic viscosity (ν) was determined from the transit time of the liquid meniscus through a Ubbelohde capillary viscosimeter supplied by Schott, capillary number I, (0.63 ± 0.01) mm internal diameter, and $K = 0.01013 \text{ mm}^2 \cdot \text{s}^{-1}$ and capillary number 0c, (0.46 ± 0.01) mm internal diameter, and $K = 0.003164 \text{ mm}^2 \cdot \text{s}^{-1}$, using eq 1.

$$\nu = K(t - \theta) \tag{1}$$

where *t* is the efflux time; *K* is the characteristic constant of the capillary viscometer; and θ is a correction value to correct end effects. Both parameters were obtained from the capillaries supplier (Schott). An electronic stopwatch with an accuracy of \pm 0.01 s was used to measure efflux times. In the measurements, a Schott-Geräte AVS 350 viscometer was used. Each measurement was repeated at least 5 times, and the uncertainty of this measurement is \pm 0.0024 mm²·s⁻¹. The dynamic viscosity (η) was obtained from the product of the kinematic viscosity (ν) and the corresponding density (ρ) of the mixture, in terms of eq 2 for each mixture composition and with a uncertainty of \pm 0.0026 mPa·s.

$$\eta = \nu \cdot \rho \tag{2}$$

Refractive Index. The refractive index was determined using an Atago RX-5000 refractometer. Before measurements, the refractometer was calibrated using distilled water in accordance with the instrument instructions. The mixtures were directly

					T_{\prime}	/K			
x_1	<i>x</i> ₂	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			A	mine Total Conc	entration $= 5 \% v$	ol			
0.0126	0.0000	1506.4	1519.7	1531.3	1541.9	1550.6	1557.5	1566.6	1571.3
0.0094	0.0018	1504.0	1517.4	1529.1	1539.3	1547.4	1554.8	1564.2	1569.0
0.0064	0.0035	1501.3	1515.1	1527.1	1537.3	1546.1	1553.5	1562.0	1567.3
0.0033	0.0048	1498.7	1511.3	1523.6	1532.8	1541.9	1549.5	1559.9	1565.8
0.0016	0.0055	1494.8	1509.4	1521.4	1532.3	1541.6	1549.3	1559.0	1564.9
0.0000	0.0064	1491.4	1506.2	1518.9	1529.4	1538.8	1546.7	1558.2	1564.3
			Ar	nine Total Conce	entration = 10 % v	70l			
0.0260	0.0000	1549.8	1560.1	1568.5	1574.8	1580.4	1584.7	1590.2	1590.8
0.0196	0.0034	1542.0	1553.0	1562.0	1568.9	1575.1	1579.8	1585.8	1587.2
0.0132	0.0067	1535.3	1546.3	1556.4	1564.4	1571.0	1576.6	1581.6	1583.8
0.0066	0.0101	1524.3	1536.3	1546.5	1555.1	1562.5	1568.8	1577.2	1580.3
0.0033	0.0116	1522.2	1534.6	1545.2	1553.7	1561.7	1567.8	1575.2	1578.7
0.0000	0.0134	1517.8	1531.0	1541.8	1550.7	1558.5	1565.0	1573.2	1577.1
			Ar	nine Total Conce	entration = 20% v	70l			
0.0565	0.0000	1635.1	1637.9	1640.0	1641.9	1642.3	1642.4	1636.4	1628.5
0.0429	0.0073	1620.6	1624.9	1628.2	1630.5	1631.2	1631.6	1628.4	1622.2
0.0285	0.0150	1602.2	1608.2	1613.1	1616.8	1619.2	1620.9	1620.4	1616.0
0.0145	0.0218	1586.8	1594.0	1600.1	1604.3	1607.9	1610.3	1611.8	1609.2
0.0078	0.0256	1580.8	1588.5	1595.0	1600.3	1604.2	1607.2	1608.3	1606.7
0.0000	0.0294	1570.1	1579.0	1586.0	1594.3	1597.0	1600.6	1604.6	1603.5

 a_{x_1} and x_2 are the mole fractions of MIPA and TEA, respectively. Standard uncertainties u are u(T) = 0.01 K, u(p) = 20 Pa, u(x) = 0.0008, and the combined expanded uncertainty U_c (level of confidence = 0.95, k = 2) is $U_c(c) = 1.2 \text{ m} \cdot \text{s}^{-1}$.

Table 5. Viscosity η of MIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 333.15) \text{ K at } p = 10^5 \text{ Pa}^a$

					T_{i}	/K			
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			Am	nine Total Conce	ntration = 5 % vo	əl			
0.0126	0.0000	1.382	1.228	1.030	0.894	0.781	0.682	0.573	0.543
0.0094	0.0018	1.379	1.221	1.026	0.892	0.774	0.672	0.578	0.542
0.0064	0.0035	1.356	1.198	1.018	0.898	0.776	0.674	0.573	0.543
0.0033	0.0048	1.346	1.181	1.012	0.898	0.776	0.690	0.564	0.541
0.0016	0.0055	1.304	1.175	1.018	0.891	0.767	0.681	0.560	0.538
0.0000	0.0064	1.304	1.141	0.998	0.872	0.765	0.664	0.555	0.536
			Am	ine Total Concer	ntration = 10 % v	ol			
0.0260	0.0000	1.731	1.488	1.273	1.122	0.990	0.868	0.720	0.636
0.0196	0.0034	1.691	1.450	1.249	1.100	0.960	0.834	0.705	0.624
0.0132	0.0067	1.660	1.405	1.241	1.082	0.950	0.831	0.705	0.623
0.0066	0.0101	1.628	1.371	1.234	1.076	0.945	0.833	0.693	0.618
0.0033	0.0116	1.593	1.340	1.199	1.052	0.919	0.806	0.680	0.627
0.0000	0.0134	1.570	1.330	1.161	1.039	0.914	0.801	0.688	0.612
			Am	ine Total Concer	ntration = 20 % v	ol			
0.0565	0.0000	2.741	2.334	1.985	1.721	1.493	1.299	1.049	0.860
0.0429	0.0073	2.650	2.196	1.908	1.661	1.441	1.263	1.027	0.840
0.0285	0.0150	2.579	2.137	1.877	1.638	1.421	1.247	1.032	0.851
0.0145	0.0218	2.512	2.100	1.840	1.590	1.395	1.234	1.014	0.835
0.0078	0.0256	2.443	2.090	1.813	1.582	1.387	1.230	0.996	0.826
0.0000	0.0294	2.400	2.070	1.789	1.559	1.369	1.204	0.988	0.820
x_1^{a} and x_2^{a} are combined expansion	the mole fractio inded uncertain	ons of MIPA an ty U _c (level of	d TEA, respect confidence = (tively. Standard 0.95, $k = 2$) is	uncertainties $U_c(\eta) = 0.002$	u are u(T) = 0. 6 mPa·s.	01 K, $u(p) = 2$	0 Pa, $u(x) = 0$.	0008, and the

injected from the stock solution stored at working temperature to avoid evaporation. The refractive index measurements were done after the liquid mixtures attained the constant temperature of the refractometer (this equipment includes an internal thermometer). This procedure was repeated at least three times, and the uncertainty of the measurement was $\pm 1.3 \cdot 10^{-4}$. The average of these readings was taken for the refractive index values. This property has not been measured at (323.15 and 333.15) K due to the importance of the evaporation process.

RESULTS AND DISCUSSION

A comparison between the experimental results for density, speed of sound, viscosity, and refractive index obtained in present work and literature data for pure components has been included in Table 2, to

Table 6. Refractive Index n_D of MIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 313.15) \text{ K at } p = 10^5 \text{ Pa}^a$

				T_{i}	/K		
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15
			Amine Total Conc	entration = 5 % vol			
0.0126	0.0000	1.3399	1.3395	1.3390	1.3384	1.3377	1.3370
0.0094	0.0018	1.3403	1.3399	1.3393	1.3388	1.3380	1.3374
0.0064	0.0035	1.3405	1.3400	1.3395	1.3390	1.3384	1.3376
0.0033	0.0048	1.3405	1.3401	1.3396	1.3390	1.3383	1.3376
0.0016	0.0055	1.3406	1.3403	1.3397	1.3392	1.3385	1.3378
0.0000	0.0064	1.3406	1.3401	1.3396	1.3390	1.3383	1.3379
			Amine Total Conce	entration = 10 % vol			
0.0260	0.0000	1.3468	1.3463	1.3460	1.3456	1.3449	1.3441
0.0196	0.0034	1.3473	1.3467	1.3463	1.3458	1.3452	1.3444
0.0132	0.0067	1.3478	1.3473	1.3467	1.3462	1.3454	1.3448
0.0066	0.0101	1.3479	1.3474	1.3469	1.3462	1.3455	1.3449
0.0033	0.0116	1.3478	1.3473	1.3468	1.3463	1.3455	1.3448
0.0000	0.0134	1.3479	1.3475	1.3469	1.3463	1.3456	1.3449
			Amine Total Conce	entration = 20 % vol			
0.0565	0.0000	1.3604	1.3598	1.3590	1.3582	1.3574	1.3564
0.0429	0.0073	1.3616	1.3608	1.3598	1.3591	1.3584	1.3574
0.0285	0.0150	1.3622	1.3614	1.3605	1.3595	1.3588	1.3580
0.0145	0.0218	1.3626	1.3617	1.3610	1.3603	1.3595	1.3586
0.0078	0.0256	1.3628	1.3622	1.3615	1.3608	1.3600	1.3592
0.0000	0.0294	1.3630	1.3624	1.3618	1.3611	1.3603	1.3594

 a_{x_1} and x_2 are the mole fractions of MIPA and TEA, respectively. Standard uncertainties u are u(T) = 0.01 K, u(p) = 20 Pa, u(x) = 0.0008, and the combined expanded uncertainty U_c (level of confidence = 0.95, k = 2) is $U_c(n_D) = 1.3 \cdot 10^{-4}$.

Table 7. Density ρ of DIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 333.15) \text{ K at } p = 10^5 \text{ Pa}^a$

					T_{i}	/K			
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			А	mine Total Conc	entration $= 5 \% v$	vol			
0.0071	0.0000	1.0026	1.0016	1.0003	0.9989	0.9972	0.9953	0.9906	0.9823
0.0057	0.0019	1.0035	1.0025	1.0013	0.9998	0.9981	0.9962	0.9918	0.9840
0.0038	0.0033	1.0046	1.0036	1.0023	1.0009	0.9992	0.9973	0.9930	0.9857
0.0018	0.0049	1.0056	1.0046	1.0034	1.0019	1.0002	0.9983	0.9942	0.9866
0.0009	0.0056	1.0060	1.0051	1.0038	1.0023	1.0006	0.9987	0.9945	0.9874
0.0000	0.0064	1.0068	1.0058	1.0046	1.0031	1.0014	0.9995	0.9950	0.9886
			Aı	nine Total Conce	entration = 10 %	vol			
0.0148	0.0000	1.0048	1.0037	1.0024	1.0008	0.9990	0.9971	0.9930	0.9876
0.0112	0.0034	1.0075	1.0064	1.005	1.0035	1.0017	0.9997	0.9954	0.9903
0.0075	0.0066	1.0098	1.0087	1.0073	1.0057	1.0039	1.0021	0.9978	0.9926
0.0040	0.0100	1.0124	1.0113	1.0099	1.0083	1.0065	1.0045	1.0001	0.9941
0.0019	0.0117	1.0135	1.0124	1.0110	1.0094	1.0077	1.0057	1.0011	0.9953
0.0000	0.0134	1.0148	1.0136	1.0122	1.0106	1.0089	1.0069	1.0023	0.9962
			Aı	nine Total Conce	entration = 20 %	vol			
0.0329	0.0000	1.0125	1.011	1.0093	1.0074	1.0053	1.0032	0.9984	0.9928
0.0246	0.0075	1.0172	1.0157	1.014	1.0122	1.0101	1.0078	1.0031	0.9975
0.0165	0.0147	1.0217	1.0202	1.0186	1.0167	1.0147	1.0124	1.0078	1.0022
0.0084	0.0221	1.0264	1.0251	1.0233	1.0215	1.0194	1.0172	1.0126	1.0069
0.0042	0.0256	1.0291	1.0276	1.0260	1.0241	1.0221	1.0199	1.0149	1.0095
0.0000	0.0294	1.0309	1.0294	1.0278	1.0261	1.0240	1.0218	1.0173	1.0112
a_{x_1} and x_2 are combined exp	the mole fract anded uncertai	ions of MIPA a inty U _c (level o	nd TEA, respect of confidence =	ctively. Standar $0.95, k = 2$ is	d uncertainties s $U_{\rm c}(\rho) = 2.10$	u are u(T) = 0 $u^{-4} \operatorname{g·cm}^{-3}.$	0.01 K, $u(p) = 2$	20 Pa, $u(x) = 0$.	.0008, and th

confirm the purity of components and the suitability of the experimental procedures to the physical properties determination.

The present work analyzes the influence of mixture composition and temperature upon density, viscosity, speed of sound, and refractive index of ternary systems formed by MIPA (1) (or DIPA) + TEA (2) + water (3), at temperatures from (288.15 to 333.15) K. Experimental mixtures maintain volume ratios between amines and

water of 5, 10, and 20 %, and the amine composition in the nonaqueous fraction was varied in the entire composition range. Tables 3 to 10 show the value of these properties determined for all of the compositions and temperatures employed in the present work.

The influence of mixture composition on density and speed of sound for these systems is shown in Figure 1. With regard to the influence of mixture composition on the value of density for

					T_{\prime}	′K			
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			А	mine Total Conc	entration $= 5 \% v$	ol			
0.0071	0.0000	1504.7	1518.4	1529.9	1539.8	1548.3	1555.2	1565.4	1570.2
0.0057	0.0019	1503.8	1517.7	1529.6	1539.3	1548.0	1555.4	1564.1	1569.2
0.0038	0.0033	1501.7	1515.6	1527.9	1538.4	1546.6	1553.8	1563.0	1568.6
0.0018	0.0049	1495.7	1509.9	1522.3	1533.1	1542.0	1549.7	1559.9	1565.7
0.0009	0.0056	1492.8	1507.2	1519.7	1530.7	1539.7	1547.3	1560.1	1565.9
0.0000	0.0064	1491.4	1506.2	1518.9	1529.4	1538.8	1546.7	1558.2	1564.3
			A	mine Total Conce	entration = 10 % v	vol			
0.0148	0.0000	1540.1	1551.4	1560.6	1567.8	1574.2	1579.1	1587.3	1588.2
0.0112	0.0034	1537.6	1548.6	1558.1	1566.1	1572.6	1577.7	1583.4	1585.3
0.0075	0.0066	1530.2	1542.2	1552.2	1560.6	1567.6	1573.2	1580.5	1583.1
0.0040	0.0100	1525.4	1537.5	1547.9	1556.3	1564.1	1569.9	1576.8	1580.0
0.0019	0.0117	1521.3	1533.6	1544.3	1553.0	1560.6	1567.1	1574.9	1578.6
0.0000	0.0134	1517.8	1531.0	1541.8	1550.7	1558.5	1565.0	1573.2	1577.1
			Ai	mine Total Conce	entration = 20 % v	vol			
0.0329	0.0000	1623.6	1627.6	1630.1	1631.6	1632.2	1631.8	1629.9	1623.1
0.0246	0.0075	1610.0	1616.3	1620.1	1622.5	1624.2	1624.7	1623.1	1617.4
0.0165	0.0147	1597.8	1604.1	1609.1	1612.8	1615.5	1617.3	1617.0	1613.1
0.0084	0.0221	1584.8	1592.5	1598.5	1603.1	1606.8	1609.3	1611.4	1609.1
0.0042	0.0256	1579.4	1587.6	1594.1	1599.3	1603.3	1606.3	1607.2	1605.7
0.0000	0.0294	1570.1	1579.0	1586.0	1592.3	1597.0	1600.6	1604.6	1603.5
		() (T) (1				a a 4 77 ()		

 a_{x_1} and x_2 are the mole fractions of MIPA and TEA, respectively. Standard uncertainties *u* are u(T) = 0.01 K, u(p) = 20 Pa, u(x) = 0.0008, and the combined expanded uncertainty U_c (level of confidence = 0.95, k = 2) is $U_c(c) = 1.2$ m·s⁻¹.

Table 9. Viscosity η of DIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 333.15) \text{ K at } p = 10^5 \text{ Pa}^a$

					T_{i}	/K			
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
			An	nine Total Conce	ntration $= 5 \%$ vo	ol			
0.0071	0.0000	1.478	1.261	1.097	0.958	0.834	0.738	0.597	0.560
0.0057	0.0019	1.438	1.245	1.072	0.931	0.813	0.708	0.579	0.542
0.0038	0.0033	1.427	1.235	1.075	0.930	0.805	0.712	0.574	0.533
0.0018	0.0049	1.368	1.185	1.026	0.892	0.769	0.673	0.565	0.529
0.0009	0.0056	1.340	1.153	1.007	0.873	0.756	0.654	0.560	0.526
0.0000	0.0064	1.304	1.141	0.998	0.872	0.765	0.664	0.555	0.520
			Am	ine Total Concer	ntration = 10 % v	ol			
0.0148	0.0000	1.834	1.610	1.370	1.211	1.046	0.914	0.775	0.667
0.0112	0.0034	1.772	1.525	1.319	1.146	1.011	0.889	0.752	0.661
0.0075	0.0066	1.749	1.509	1.310	1.133	1.009	0.889	0.729	0.650
0.0040	0.0100	1.730	1.465	1.282	1.126	0.997	0.859	0.724	0.644
0.0019	0.0117	1.652	1.444	1.267	1.116	0.972	0.848	0.712	0.627
0.0000	0.0134	1.570	1.330	1.161	1.039	0.914	0.801	0.688	0.612
			Am	ine Total Concer	$ration = 20 \% v_0$	ol			
0.0329	0.0000	3.378	2.803	2.363	2.080	1.803	1.540	1.200	0.985
0.0246	0.0075	3.191	2.664	2.248	1.915	1.642	1.429	1.140	0.970
0.0165	0.0147	2.940	2.460	2.051	1.762	1.560	1.324	1.100	0.927
0.0084	0.0221	2.729	2.315	1.977	1.706	1.507	1.308	1.050	0.892
0.0042	0.0256	2.600	2.210	1.910	1.660	1.454	1.260	1.030	0.848
0.0000	0.0294	2.400	2.070	1.789	1.570	1.369	1.204	0.988	0.820
a_{x_1} and x_2 are	the mole fractio	ns of MIPA an	d TEA, respect	tively. Standard	uncertainties <i>i</i>	u are $u(T) = 0$.	01 K, $u(p) = 2$	0 Pa, $u(x) = 0$.	0008, and the

combined expanded uncertainty U_c (level of confidence = 0.95, k = 2) is $U_c(\eta) = 0.0026$ mPa·s.

both systems, an increase in TEA composition in the liquid mixture produces an increase in density value, with a higher slope for the MIPA + TEA + water system. The high influence of TEA upon the density value is in agreement with previous studies.¹⁶ The same behavior has been observed for all temperatures studied for these systems. The experimental

results obtained for speed of sound show that the behavior for each analyzed system has been similar. The speed of sound data decreases when mixture is enriched in TEA.¹⁶

The influence of mixture composition on the viscosity and refractive index for these systems is shown in Figure 2. In relation to the influence of mixture composition on the value of

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Table 10. Refractive Index n_D of DIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 313.15) \text{ K at } p = 10^5 \text{ Pa}^a$

				T,	/K		
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15
			Amine Total Conc	entration = 5 % vol			
0.0071	0.0000	1.3405	1.3401	1.3396	1.3390	1.3383	1.3377
0.0057	0.0019	1.3410	1.3406	1.3401	1.3395	1.3388	1.3382
0.0038	0.0033	1.3409	1.3405	1.3400	1.3394	1.3388	1.3381
0.0018	0.0049	1.3408	1.3403	1.3398	1.3392	1.3385	1.3380
0.0009	0.0056	1.3407	1.3402	1.3396	1.3389	1.3383	1.3378
0.0000	0.0064	1.3406	1.3401	1.3396	1.3390	1.3383	1.3379
			Amine Total Conce	entration = 10 % vol			
0.0148	0.0000	1.3470	1.3465	1.3460	1.3454	1.3446	1.3439
0.0112	0.0034	1.3477	1.3472	1.3467	1.3461	1.3454	1.3446
0.0075	0.0066	1.3477	1.3472	1.3467	1.3460	1.3454	1.3446
0.0040	0.0100	1.3481	1.3475	1.3469	1.3463	1.3456	1.3447
0.0019	0.0117	1.3478	1.3473	1.3467	1.3461	1.3454	1.3446
0.0000	0.0134	1.3479	1.3475	1.3469	1.3463	1.3456	1.3449
			Amine Total Conce	entration = 20 % vol			
0.0329	0.0000	1.3626	1.3619	1.3613	1.3606	1.3598	1.3589
0.0246	0.0075	1.3630	1.3622	1.3617	1.3609	1.3600	1.3592
0.0165	0.0147	1.3630	1.3623	1.3616	1.3610	1.3601	1.3592
0.0084	0.0221	1.3631	1.3625	1.3618	1.3612	1.3604	1.3596
0.0042	0.0256	1.3631	1.3625	1.3618	1.3611	1.3604	1.3596
0.0000	0.0294	1.3630	1.3624	1.3618	1.3611	1.3603	1.3594

 a_{x_1} and x_2 are the mole fractions of MIPA and TEA, respectively. Standard uncertainties *u* are u(T) = 0.01 K, u(p) = 20 Pa, u(x) = 0.0008, and the combined expanded uncertainty U_c (level of confidence = 0.95, k = 2) is $U_c(n_D) = 1.3 \cdot 10^{-4}$.



Figure 1. Influence of mixture composition on density and speed of sound. MIPA (1) + TEA (2) + water (3) system: \blacklozenge , density; \blacktriangle , speed of sound. DIPA (1) + TEA (2) + water (3) system: \blacksquare , density; \times , speed of sound. T = 313.15 K.

viscosity for both systems, the viscosity shows a low decrease in its value when TEA composition increases in the mixture.

For refractive index values, the behavior for both systems is very similar, and this property takes similar values observing a noninfluence of TEA composition and the use of MIPA and DIPA. The behavior observed for all of the physical properties is in agreement with previous studies that analyze other ternary systems based on amine blends.^{10,11}

Another interesting aspect in this kind of characterization is the influence of temperature upon the behavior of this system and over the different physical properties. Figure 3 shows the influence of temperature in the behavior of speed of sound and viscosity. An increase in temperature produces opposite effects on speed of sound and viscosity. The obtained behavior for speed of sound shows an increase in the value of this property when temperature increases. However, viscosity shows a decrease in the value when the temperature increased.



Figure 2. Influence of mixture composition on viscosity and refractive index. MIPA (1) + TEA (2) + water (3) system: \blacklozenge , viscosity; \blacktriangle , refractive index. DIPA (1) + TEA (2) + water (3) system: \blacksquare , viscosity; ×, refractive index. *T* = 308.15 K.



Figure 3. Influence of temperature on speed of sound and viscosity for MIPA (1) + TEA (2) + water (3) systems: \blacklozenge , speed sound; \blacksquare , viscosity. $x_2 = 0.0018$. Amine total concentration = 5 % vol.

Figure 4 shows the influence of total amine content and the relation between the blended amines upon the viscosity value for the MIPA + TEA + water system. The effect caused by the amine ratio shows the same behavior previously commented in



Figure 4. Influence of the total composition of amine on viscosity for MIPA (1) + TEA (2) + water (3). Amine/water volume relation: \blacklozenge , 5 %; \blacksquare , 10 %; \blacktriangle , 20 %. *T* = 313.15 K.

Figure 2, but a higher influence of TEA composition upon viscosity, that causes a decrease, is observed for the most concentrated system in amines (20 %). Also, an increase in the total amines concentration in the mixture produces a clear increase in the value of viscosity for all of the MIPA/TEA relations.

The excess molar volumes of mixtures (V^{E}) were calculated from density measures by applying eq 3

$$V^{\rm E} = \sum_{i=1}^{3} x_i M_i (\rho^{-1} - \rho_i^{-1})$$
(3)

Table 12. Excess Volume V^{E} of DIPA (1) + TEA (2) + Water (3)
from $T = (323.15 \text{ to } 333.15) \text{ K}^a$

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		T_{c}	/K
x_1	x_2	323.15	333.15
	Amine Total Con	centration = 5 % vol	
0.0071	0.0000	-0.0518	-0.0128
0.0057	0.0019	-0.0586	-0.0038
0.0038	0.0033	-0.0679	-0.0229
0.0018	0.0049	-0.0766	-0.0263
0.0009	0.0056	-0.0756	-0.0348
0.0000	0.0064	-0.0778	-0.0503
	Amine Total Conc	entration = 10 % vol	l
0.0148	0.0000	-0.1040	-0.0962
0.0112	0.0034	-0.1205	-0.1186
0.0075	0.0066	-0.1375	-0.1337
0.0040	0.0100	-0.1507	-0.1317
0.0019	0.0117	-0.1541	-0.1389
0.0000	0.0134	-0.1610	-0.1402
	Amine Total Conc	entration = 20 % vol	l
0.0329	0.0000	-0.2330	-0.2235
0.0246	0.0075	-0.2653	-0.2558
0.0165	0.0147	-0.2989	-0.2895
0.0084	0.0221	-0.3333	-0.3220
0.0042	0.0256	-0.3485	-0.3433
0.0000	0.0294	-0.3641	-0.3447
x_1 and x_2 are t	he mole fractions	of MIPA and TE	A. respectively.

where $x_{ij} M_{ij}$ and ρ_i are the mole fractions, molecular weights, and densities of pure components, respectively. DIPA shows a low solubility in water, and for this reason the excess volume corresponding to systems with DIPA has been only calculated for high temperatures. The corresponding excess molar volume uncertainty was $\pm 0.001 \text{ cm}^3 \cdot \text{mol}^{-1}$.

The calculated values corresponding to excess molar volumes for the experimental systems analyzed in the present work are

Table 11. Excess Volume V^{E} of MIPA (1) + TEA (2) + Water (3) from $T = (288.15 \text{ to } 333.15) \text{ K}^{a}$

		T/K							
x_1	x_2	288.15	293.15	298.15	303.15	308.15	313.15	323.15	333.15
Amine Total Concentration = 5 % vol									
0.0126	0.0000	-0.0485	-0.0505	-0.0527	-0.0547	-0.0566	-0.0584	-0.0632	-0.0640
0.0094	0.0018	-0.0560	-0.0573	-0.0587	-0.0600	-0.0614	-0.0626	-0.0673	-0.0672
0.0064	0.0035	-0.0678	-0.0684	-0.0691	-0.0697	-0.0704	-0.0710	-0.0735	-0.0532
0.0033	0.0048	-0.0801	-0.0797	-0.0797	-0.0796	-0.0796	-0.0795	-0.0786	-0.0652
0.0016	0.0055	-0.0828	-0.0820	-0.0815	-0.0810	-0.0807	-0.0804	-0.0812	-0.0503
0.0000	0.0064	-0.0866	-0.0854	-0.0844	-0.0836	-0.0829	-0.0822	-0.0778	-0.0503
Amine Total Concentration = 10 % vol									
0.0260	0.0000	-0.1133	-0.1165	-0.1197	-0.1228	-0.1259	-0.1289	-0.1333	-0.1355
0.0196	0.0034	-0.1353	-0.1371	-0.1391	-0.1410	-0.1431	-0.1450	-0.1453	-0.1456
0.0132	0.0067	-0.1623	-0.1625	-0.1630	-0.1637	-0.1645	-0.1653	-0.1501	-0.1365
0.0066	0.0101	-0.1609	-0.1600	-0.1594	-0.1589	-0.1587	-0.1586	-0.1592	-0.1401
0.0033	0.0116	-0.1662	-0.1643	-0.1629	-0.1617	-0.1607	-0.1600	-0.1610	-0.1410
0.0000	0.0134	-0.1756	-0.1729	-0.1707	-0.1687	-0.1671	-0.1656	-0.1610	-0.1402
Amine Total Concentration $= 20 \%$ vol									
0.0565	0.0000	-0.2905	-0.2927	-0.2954	-0.2983	-0.3014	-0.3044	-0.3090	-0.3141
0.0429	0.0073	-0.3253	-0.3259	-0.3271	-0.3286	-0.3304	-0.3320	-0.3344	-0.3382
0.0285	0.0150	-0.3410	-0.3399	-0.3395	-0.3395	-0.3398	-0.3404	-0.3395	-0.3413
0.0145	0.0218	-0.3643	-0.3606	-0.3578	-0.3555	-0.3537	-0.3522	-0.3447	-0.3363
0.0078	0.0256	-0.3640	-0.3589	-0.3548	-0.3513	-0.3483	-0.3458	-0.3441	-0.3416
0.0000	0.0294	-0.3573	-0.3510	-0.3457	-0.3410	-0.3370	-0.3334	-0.3333	-0.3149

 ${}^{a}x_{1}$ and x_{2} are the mole fractions of MIPA and TEA, respectively.

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shown in Tables 11 and 12. These data show, for analyzed systems, negative values of excess molar volume for all of the compositions included in the studied ranges. This behavior is in agreement with previous studies that analyze the binary aqueous mixtures of the components used in present work.^{13–15}

CONCLUSIONS

Different physical properties have been determined for the systems MIPA (or DIPA) + TEA + water, and the presence of TEA produces an increase in density and refractive index, but on the other hand, a low influence of TEA in comparison with MIPA (or DIPA) was observed in relation to speed of sound and viscosity. The effect of temperature in these mixtures produces a decrease in the magnitude of all properties except for speed of sound. The excess molar volume shows negative values for all compositions and temperatures.

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Notes

The authors declare no competing financial interest.

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